

## LM78L00 Series 3-Terminal Positive Voltage Regulators

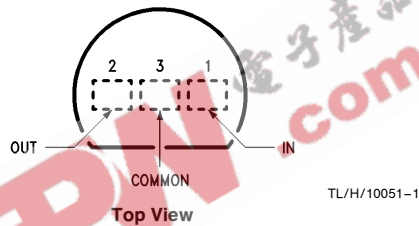
### General Description

The LM78L00 series of 3-terminal positive voltage regulators employ internal current-limiting and thermal shutdown, making them essentially indestructible. If adequate heat sinking is provided, they can deliver up to 100 mA output current. They are intended as fixed voltage regulators in a wide range of applications including local (on-card) regulation for elimination of noise and distribution problems associated with single-point regulation. In addition, they can be used with power pass elements to make high current voltage regulators. The LM78L00, used as a Zener diode/resistor combination replacement, offers an effective output impedance improvement of typically two orders of magnitude, along with lower quiescent current and lower noise.

### Features

- Output current up to 100 mA
- No external components
- Internal thermal overload protection
- Internal short circuit current-limiting
- Available in JEDEC TO-92
- Output Voltages of 5.0V, 6.2V, 8.2V, 9.0V, 12V, 15V
- Output voltage tolerances of  $\pm 5\%$  over the temperature range

### Connection Diagram



Order Number LM78L05ACZ, LM78L09ACZ,  
LM78L12ACZ, LM78L15ACZ, LM78L62ACZ or LM78L82ACZ  
See NS Package Number Z03A

LM78L00 Series 3-Terminal Positive Voltage Regulators



## LM78L62AC

### Electrical Characteristics

$0^{\circ}\text{C} \leq T_A \leq +125^{\circ}\text{C}$ ,  $V_I = 12\text{V}$ ,  $I_O = 40\text{ mA}$ ,  $C_I = 0.33\ \mu\text{F}$ ,  $C_O = 0.1\ \mu\text{F}$ , unless otherwise specified (Note 1)

Symbol	Parameter	Conditions	Min	Typ	Max	Units	
$V_O$	Output Voltage	$T_J = 25^{\circ}\text{C}$	5.95	6.2	6.45	V	
$V_{R\text{ LINE}}$	Line Regulation	$T_J = 25^{\circ}\text{C}$				mV	
		$8.5\text{V} \leq V_I \leq 20\text{V}$		65	175		
				55	125		
$V_{R\text{ LOAD}}$	Load Regulation	$T_J = 25^{\circ}\text{C}$				mV	
		$1.0\text{ mA} \leq I_O \leq 100\text{ mA}$		13	80		
				6.0	40		
$V_O$	Output Voltage (Note 2)	$8.5\text{V} \leq V_I \leq 20\text{V}$				V	
		$1.0\text{ mA} \leq I_O \leq 40\text{ mA}$	5.90		6.5		
		$8.5\text{V} \leq V_I \leq V_{\text{Max}}$				6.5	
		$1.0\text{ mA} \leq I_O \leq 70\text{ mA}$	5.90				
$I_Q$	Quiescent Current			2.0	5.5	mA	
$\Delta I_Q$	Quiescent Current Change	With Line	$8.0\text{V} \leq V_I \leq 20\text{V}$			1.5	mA
		With Load	$1.0\text{ mA} \leq I_O \leq 40\text{ mA}$			0.1	
$N_O$	Noise	$T_A = 25^{\circ}\text{C}$ , $10\text{ Hz} \leq f \leq 100\text{ kHz}$		50		$\mu\text{V}$	
$\Delta V_I / \Delta V_O$	Ripple Rejection	$f = 120\text{ Hz}$ , $10\text{V} \leq V_I \leq 20\text{V}$ , $T_J = 25^{\circ}\text{C}$	40	46		dB	
$V_{\text{DO}}$	Dropout Voltage	$T_J = 25^{\circ}\text{C}$		1.7		V	
$I_{\text{pk}} / I_{\text{OS}}$	Peak Output/Output Short Circuit Current	$T_J = 25^{\circ}\text{C}$		140		mA	
$\Delta V_O / \Delta T$	Average Temperature Coefficient of Output Voltage	$I_O = 5.0\text{ mA}$		-0.75		$\text{mV}/^{\circ}\text{C}$	

## LM78L82AC

### Electrical Characteristics

$0^{\circ}\text{C} \leq T_A \leq +125^{\circ}\text{C}$ ,  $V_I = 14\text{V}$ ,  $I_O = 40\text{ mA}$ ,  $C_I = 0.33\ \mu\text{F}$ ,  $C_O = 0.1\ \mu\text{F}$ , unless otherwise specified (Note 1)

Symbol	Parameter	Conditions	Min	Typ	Max	Units	
$V_O$	Output Voltage	$T_J = 25^{\circ}\text{C}$	7.87	8.2	8.53	V	
$V_{R\text{ LINE}}$	Line Regulation	$T_J = 25^{\circ}\text{C}$				mV	
		$11\text{V} \leq V_I \leq 23\text{V}$		80	175		
				70	125		
$V_{R\text{ LOAD}}$	Load Regulation	$T_J = 25^{\circ}\text{C}$				mA	
		$1.0\text{ mA} \leq I_O \leq 100\text{ mA}$		15	80		
				8.0	40		
$V_O$	Output Voltage (Note 2)	$11\text{V} \leq V_I \leq 23\text{V}$				V	
		$1.0\text{ mA} \leq I_O \leq 40\text{ mA}$	7.8		8.5		
		$11\text{V} \leq V_I \leq V_{\text{Max}}$				8.6	
		$1.0\text{ mA} \leq I_O \leq 70\text{ mA}$	7.8				
$I_Q$	Quiescent Current			2.1	5.5	mA	
$\Delta I_Q$	Quiescent Current Change	With Line	$12\text{V} \leq V_I \leq 23\text{V}$			1.5	mA
		With Load	$1.0\text{ mA} \leq I_O \leq 40\text{ mA}$			0.1	
$N_O$	Noise	$T_A = 25^{\circ}\text{C}$ , $10\text{ Hz} \leq f \leq 100\text{ kHz}$		60		$\mu\text{V}$	
$\Delta V_I / \Delta V_O$	Ripple Rejection	$f = 120\text{ Hz}$ , $12\text{V} \leq V_I \leq 22\text{V}$ , $T_J = 25^{\circ}\text{C}$	39	45		dB	
$V_{\text{DO}}$	Dropout Voltage	$T_J = 25^{\circ}\text{C}$		1.7		V	
$I_{\text{pk}} / I_{\text{OS}}$	Peak Output/Output Short Circuit Current	$T_J = 25^{\circ}\text{C}$		140		mA	
$\Delta V_O / \Delta T$	Average Temperature Coefficient of Output Voltage	$I_O = 5.0\text{ mA}$		-0.8		$\text{mV}/^{\circ}\text{C}$	

**Note 1:** The maximum steady state usable output current and input voltage are very dependent on the heat sinking and/or lead length of the package. The data above represent pulse test conditions with junction temperatures as indicated at the initiation of tests.

**Note 2:** Power Dissipation  $\leq 0.75\text{W}$ .

## LM78L09AC

### Electrical Characteristics

$0^{\circ}\text{C} \leq T_A \leq +125^{\circ}\text{C}$ ,  $V_I = 15\text{V}$ ,  $I_O = 40\text{ mA}$ ,  $C_I = 0.33\ \mu\text{F}$ ,  $C_O = 0.1\ \mu\text{F}$ , unless otherwise specified (Note 1)

Symbol	Parameter	Conditions	Min	Typ	Max	Units	
$V_O$	Output Voltage	$T_J = 25^{\circ}\text{C}$	8.64	9.0	9.36	V	
$V_{R\text{ LINE}}$	Line Regulation	$T_J = 25^{\circ}\text{C}$		90	200	mV	
		$11.5\text{V} \leq V_I \leq 24\text{V}$					
				100	150		
$V_{R\text{ LOAD}}$	Load Regulation	$T_J = 25^{\circ}\text{C}$		20	90	mV	
		$1.0\text{ mA} \leq I_O \leq 100\text{ mA}$					
				10	45		
$V_O$	Output Voltage (Note 2)	$11.5\text{V} \leq V_I \leq 24\text{V}$	$1.0\text{ mA} \leq I_O \leq 40\text{ mA}$	8.55		9.45	V
		$11.5\text{V} \leq V_I \leq V_{\text{Max}}$	$1.0\text{ mA} \leq I_O \leq 70\text{ mA}$	8.55		9.45	
$I_Q$	Quiescent Current			2.1	5.5	mA	
$\Delta I_Q$	Quiescent Current Change	With Line	$11.5\text{V} \leq V_I \leq 24\text{V}$			1.5	mA
		With Load	$1.0\text{ mA} \leq I_O \leq 40\text{ mA}$			0.1	
$N_O$	Noise	$T_A = 25^{\circ}\text{C}$ , $10\text{ Hz} \leq f \leq 100\text{ kHz}$		70		$\mu\text{V}$	
$\Delta V_I / \Delta V_O$	Ripple Rejection	$f = 120\text{ Hz}$ , $15\text{V} \leq V_I \leq 25\text{V}$ , $T_J = 25^{\circ}\text{C}$	38	44		dB	
$V_{\text{DO}}$	Dropout Voltage	$T_J = 25^{\circ}\text{C}$		1.7		V	
$I_{\text{pk}} / I_{\text{OS}}$	Peak Output/Output Short Circuit Current	$T_J = 25^{\circ}\text{C}$		140		mA	
$\Delta V_O / \Delta T$	Average Temperature Coefficient of Output Voltage	$I_O = 5.0\text{ mA}$		-0.9		$\text{mV}/^{\circ}\text{C}$	

## LM78L12AC

### Electrical Characteristics

$0^{\circ}\text{C} \leq T_A \leq +125^{\circ}\text{C}$ ,  $V_I = 19\text{V}$ ,  $I_O = 40\text{ mA}$ ,  $C_I = 0.33\ \mu\text{F}$ ,  $C_O = 0.1\ \mu\text{F}$ , unless otherwise specified (Note 1)

Symbol	Parameter	Conditions	Min	Typ	Max	Units	
$V_O$	Output Voltage	$T_J = 25^{\circ}\text{C}$	11.5	12	12.5	V	
$V_{R\text{ LINE}}$	Line Regulation	$T_J = 25^{\circ}\text{C}$		120	250	mV	
		$14.5\text{V} \leq V_I \leq 27\text{V}$					
				100	200		
$V_{R\text{ LOAD}}$	Load Regulation	$T_J = 25^{\circ}\text{C}$		20	100	mV	
		$1.0\text{ mA} \leq I_O \leq 100\text{ mA}$					
				10	50		
$V_O$	Output Voltage (Note 2)	$14.5\text{V} \leq V_I \leq 27\text{V}$	$1.0\text{ mA} \leq I_O \leq 40\text{ mA}$	11.4		12.6	V
		$14.5\text{V} \leq V_I \leq V_{\text{Max}}$	$1.0\text{ mA} \leq I_O \leq 70\text{ mA}$	11.4		12.6	
$I_Q$	Quiescent Current			2.1	5.5	mA	
$\Delta I_Q$	Quiescent Current Change	With Line	$16\text{V} \leq V_I \leq 27\text{V}$			1.5	mA
		With Load	$1.0\text{ mA} \leq I_O \leq 40\text{ mA}$			0.1	
$N_O$	Noise	$T_A = 25^{\circ}\text{C}$ , $10\text{ Hz} \leq f \leq 100\text{ kHz}$		80		$\mu\text{V}$	
$\Delta V_I / \Delta V_O$	Ripple Rejection	$f = 120\text{ Hz}$ , $15\text{V} \leq V_I \leq 25\text{V}$ , $T_J = 25^{\circ}\text{C}$	37	42		dB	
$V_{\text{DO}}$	Dropout Voltage	$T_J = 25^{\circ}\text{C}$		1.7		V	
$I_{\text{pk}} / I_{\text{OS}}$	Peak Output/Output Short Circuit Current	$T_J = 25^{\circ}\text{C}$		140		mA	
$\Delta V_O / \Delta T$	Average Temperature Coefficient of Output Voltage	$I_O = 5.0\text{ mA}$		-1.0		$\text{mV}/^{\circ}\text{C}$	

**Note 1:** The maximum steady state usable output current and input voltage are very dependent on the heat sinking and/or lead length of the package. The data above represent pulse test conditions with junction temperatures as indicated at the initiation of tests.

**Note 2:** Power Dissipation  $\leq 0.75\text{W}$ .

## LM78L15AC Electrical Characteristics

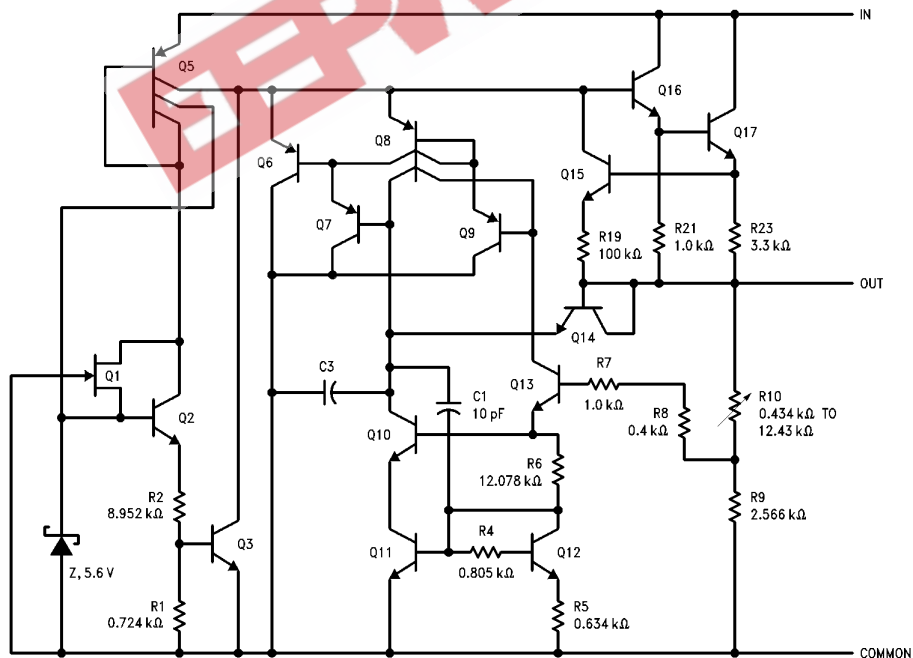
$0^{\circ}\text{C} \leq T_A \leq +125^{\circ}\text{C}$ ,  $V_I = 23\text{V}$ ,  $I_O = 40\text{ mA}$ ,  $C_I = 0.33\ \mu\text{F}$ ,  $C_O = 0.1\ \mu\text{F}$ , unless otherwise specified (Note 1)

Symbol	Parameter	Conditions	Min	Typ	Max	Units	
$V_O$	Output Voltage	$T_J = 25^{\circ}\text{C}$	14.4	15	15.6	V	
$V_{R\text{ LINE}}$	Line Regulation	$T_J = 25^{\circ}\text{C}$	$17.5\text{V} \leq V_I \leq 30\text{V}$		130	300	mV
			$20\text{V} \leq V_I \leq 30\text{V}$		110	250	
$V_{R\text{ LOAD}}$	Load Regulation	$T_J = 25^{\circ}\text{C}$	$1.0\text{ mA} \leq I_O \leq 100\text{ mA}$		25	150	mV
			$1.0\text{ mA} \leq I_O \leq 40\text{ mA}$		12	75	
$V_O$	Output Voltage (Note 2)	$17.5\text{V} \leq V_I \leq 30\text{V}$	$1.0\text{ mA} \leq I_O \leq 40\text{ mA}$	14.25		15.75	V
		$17.5\text{V} \leq V_I \leq V_{\text{Max}}$	$1.0\text{ mA} \leq I_O \leq 70\text{ mA}$	14.25		15.75	
$I_Q$	Quiescent Current			2.2	5.5	mA	
$\Delta I_Q$	Quiescent Current Change	With Line	$20\text{V} \leq V_I \leq 30\text{V}$			1.5	mA
		With Load	$1.0\text{ mA} \leq I_O \leq 40\text{ mA}$			0.1	
$N_O$	Noise	$T_A = 25^{\circ}\text{C}$ , $10\text{ Hz} \leq f \leq 100\text{ kHz}$		90		$\mu\text{V}$	
$\Delta V_I / \Delta V_O$	Ripple Rejection	$f = 120\text{ Hz}$ , $18.5\text{V} \leq V_I \leq 28.5\text{V}$ , $T_J = 25^{\circ}\text{C}$	34	39		dB	
$V_{\text{DO}}$	Dropout Voltage	$T_J = 25^{\circ}\text{C}$		1.7		V	
$I_{\text{pk}} / I_{\text{OS}}$	Peak Output/Output Short Circuit Current	$T_J = 25^{\circ}\text{C}$		140		mA	
$\Delta V_O / \Delta T$	Average Temperature Coefficient of Output Voltage	$I_O = 5.0\text{ mA}$		-1.3		$\text{mV}/^{\circ}\text{C}$	

**Note 1:** The maximum steady state usable output current and input voltage are very dependent on the heat sinking and/or lead length of the package. The data above represent pulse test conditions with junction temperatures as indicated at the initiation of tests.

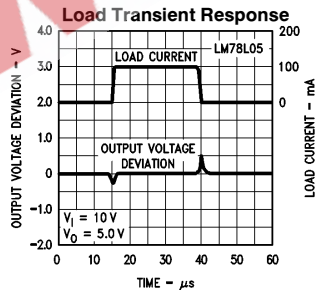
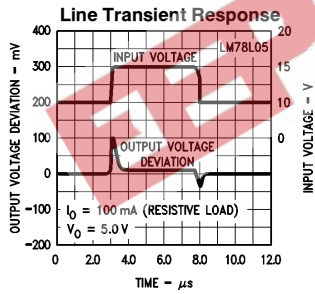
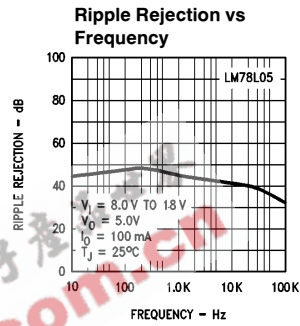
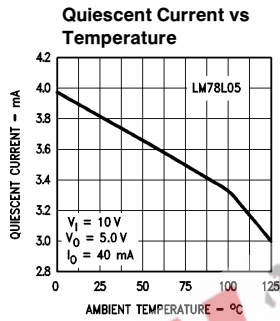
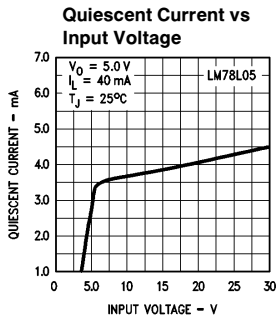
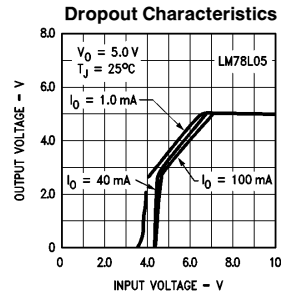
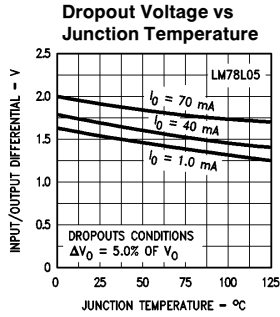
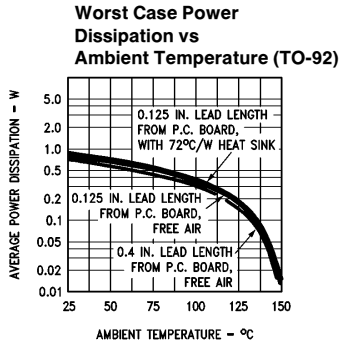
**Note 2:** Power Dissipation  $\leq 0.75\text{W}$ .

### Equivalent Circuit



TL/H/10051-2

# Typical Performance Characteristics



Note: Other LM78L00 Series devices have similar curves.

TL/H/10051-3

## Design Considerations

The LM78L series regulators have thermal overload protection from excessive power, internal short-circuit protection which limits each circuit's maximum current, and output transistor safe-area protection for reducing the output current as the voltage across each pass transistor is increased. Although the internal power dissipation is limited, the junction temperature must be kept below the maximum specified temperature (125°C) in order to meet data sheet specifications. To calculate the maximum junction temperature or heat sink required, the following thermal resistance values should be used:

Package	Typ $\theta_{JC}$	Max $\theta_{JC}$	Typ $\theta_{JA}$	Max $\theta_{JA}$
TO-92			160	160

## Thermal Considerations

The TO-92 molded package is capable of unusually high power dissipation due to the lead frame design. However, its thermal capabilities are generally overlooked because of a lack of understanding of the thermal paths from the semiconductor junction to ambient temperature. While thermal resistance is normally specified for the device mounted 1 cm above an infinite heat sink, very little has been mentioned of the options available to improve on the conservatively rated thermal capability.

An explanation of the thermal paths of the TO-92 will allow the designer to determine the thermal stress he is applying in any given application.

## The TO-92 Package

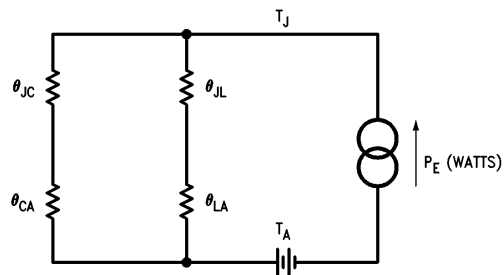
The TO-92 package thermal paths are complex. In addition to the path through the molding compound to ambient temperature, there is another path through the leads, in parallel with the case path, to ambient temperature, as shown in Figure 1.

The total thermal resistance in this model is then:

$$\theta_{JA} = \frac{(\theta_{JC} + \theta_{CA})(\theta_{JL} + \theta_{LA})}{\theta_{JC} + \theta_{CA} + \theta_{JL} + \theta_{LA}} \quad (1)$$

Where:

- $\theta_{JC}$  = thermal resistance of the case between the regulator die and a point on the case directly above the die location.
- $\theta_{CA}$  = thermal resistance between the case and air at ambient temperature.
- $\theta_{JL}$  = thermal resistance from regulator die through the input lead to a point  $1/16$  inch below the regulator case.
- $\theta_{LA}$  = total thermal resistance of the input/output ground leads to ambient temperature.
- $\theta_{JA}$  = junction to ambient thermal resistance.



TL/H/10051-4

FIGURE 1. TO-92 Thermal Equivalent Circuit

## Methods of Heat Sinking

With two external thermal resistances in each leg of a parallel network available to the circuit designer as variables, he can choose the method of heat sinking most applicable to his particular situation. To demonstrate, consider the effect of placing a small 72 °C/W flag type heat sink, such as the Staver F1-7D-2, on the LM78L00 molded case. The heat sink effectively replaces the  $\theta_{CA}$  (Figure 2) and the new thermal resistance,  $\theta'_{JA}$ , equals 145 °C/W (assuming, 0.125 inch lead length).

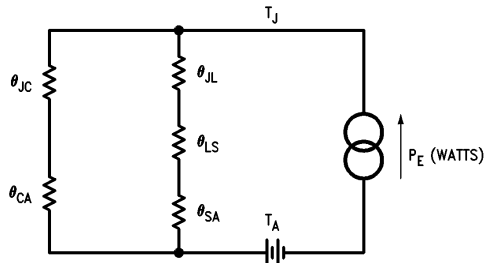
The net change of 15 °C/W increases the allowable power dissipation to 0.86W with a minimal inserted cost. A still further decrease in  $\theta_{JA}$  could be achieved by using a heat sink rated at 46 °C/W, such as the Staver FS-7A. Also, if the case sinking does not provide an adequate reduction in total  $\theta_{JA}$ , the other external thermal resistance,  $\theta_{LA}$ , may be reduced by shortening the lead length from package base to mounting medium. However, one point must be kept in mind. The lead thermal path includes a thermal resistance,  $\theta_{SA}$ , from the leads at the mounting point to ambient, that is, the mounting medium.  $\theta_{LA}$  is then equal to  $\theta_{LS} + \theta_{SA}$ . The new model is shown in Figure 2.

In the case of a socket,  $\theta_{SA}$  could be as high as 270 °C/W, thus causing a net increase in  $\theta_{JA}$  and a consequent decrease in the maximum dissipation capability. Shortening the lead length may return the net  $\theta_{JA}$  to the original value, but lead sinking would not be accomplished.

In those cases where the regulator is inserted into a copper clad printed circuit board, it is advantageous to have a maximum area of copper at the entry points of the leads. While it would be desirable to rigorously define the effect of PC board copper, the real world variables are too great to allow anything more than a few general observations.

## Methods of Heat Sinking (Continued)

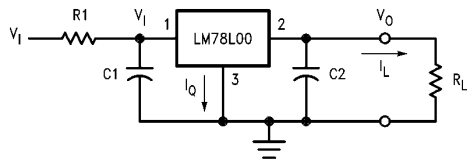
The best analogy for PC board copper is to compare it with parallel resistors. Beyond some point, additional resistors are not significantly effective; beyond some point, additional copper area is not effective.



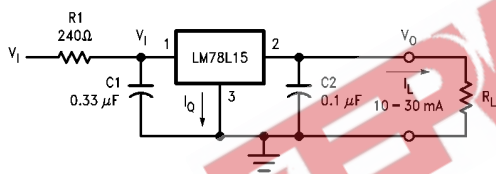
TL/H/10051-5

FIGURE 2. TO-92 Thermal Equivalent Circuit (Lead at other than Ambient Temperature)

## High Dissipation Applications



TL/H/10051-6



TL/H/10051-7

Where it is necessary to operate a LM78L00 regulator with a large input/output differential voltage, the addition of series resistor R1 will extend the output current range of the device by sharing the total power dissipation between R1 and the regulator.

$$R1 = \frac{V_{I \text{ Min}} - V_O - 2.0V}{I_{L \text{ Max}} + I_Q} \quad (2)$$

where:

$I_Q$  is the regulator quiescent current.

Regulator power dissipation at maximum input voltage and maximum load current is now

$$P_{D \text{ Max}} = (V_1 - V_O) I_{L \text{ Max}} + V_1 I_Q \quad (3)$$

where:

$$V_1 = V_{I \text{ Max}} - (I_{L \text{ Max}} + I_Q) R1$$

The presence of R1 will affect load regulation according to the equation:

$$\begin{aligned} \text{Load regulation (at constant } V_1) &= \text{load regulation (at constant } V_1) \\ &+ \text{line regulation (mV per V)} \\ &\times (R1) \times (\Delta I_L). \end{aligned} \quad (4)$$

As an example, consider a 15V regulator with a supply voltage of  $30 \pm 5.0V$ , required to supply a maximum load current of 30 mA.  $I_Q$  is 4.3 mA, and minimum load current is to be 10 mA.

$$R1 = \frac{25 - 15 - 2}{30 + 4.3} = \frac{8}{34.3} \approx 240\Omega \quad (5)$$

$$V_1 = 35 - (30 + 4.3) 0.24 = 35 - 8.2 = 26.8V$$

$$P_{D \text{ Max}} = (26.8 - 15) 30 + 26.8 (4.3)$$

$$= 354 + 115$$

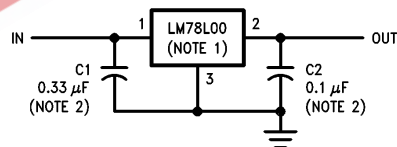
$$= 470 \text{ mW, which permit operation up to}$$

$$70^\circ\text{C in most applications.}$$

Line regulation of this circuit is typically 110 mV for an input range of 25V-35V at a constant load current; i.e. 11 mV/V.

$$\begin{aligned} \text{Load regulation} &= \text{constant } V_1 \text{ load regulation} \\ &(\text{typically } 10 \text{ mV, } 10 \text{ mA-30 mA } I_L) \\ &+ (11 \text{ mV/V}) \times 0.24 \times 20 \text{ mA} \\ &(\text{typically } 53 \text{ mV}) \\ &= 63 \text{ mV for a load current change of} \\ &20 \text{ mA at a constant } V_1 \text{ of } 30V. \end{aligned} \quad (6)$$

## Typical Applications



TL/H/10051-8

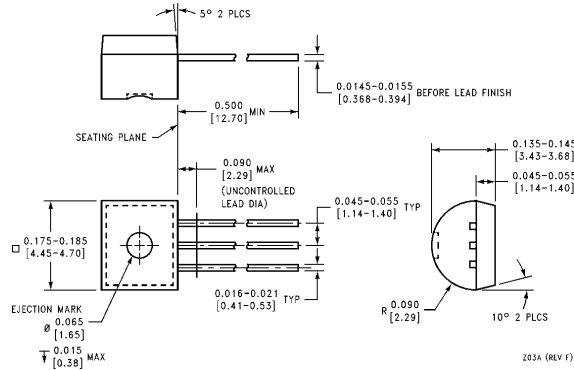
**Note 1:** To specify an output voltage, substitute voltage value for "00".

**Note 2:** Bypass capacitors are recommended for optimum stability and transient response and should be located as close as possible to the regulator.



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**Physical Dimensions** inches (millimeters)



**Order Number LM78L05ACZ, LM78L09ACZ,  
LM78L12ACZ, LM78L15ACZ, LM78L62ACZ or LM78L82ACZ  
NS Package Number Z03A**



**LIFE SUPPORT POLICY**

NATIONAL'S PRODUCTS ARE NOT AUTHORIZED FOR USE AS CRITICAL COMPONENTS IN LIFE SUPPORT DEVICES OR SYSTEMS WITHOUT THE EXPRESS WRITTEN APPROVAL OF THE PRESIDENT OF NATIONAL SEMICONDUCTOR CORPORATION. As used herein:

1. Life support devices or systems are devices or systems which, (a) are intended for surgical implant into the body, or (b) support or sustain life, and whose failure to perform, when properly used in accordance with instructions for use provided in the labeling, can be reasonably expected to result in a significant injury to the user.
2. A critical component is any component of a life support device or system whose failure to perform can be reasonably expected to cause the failure of the life support device or system, or to affect its safety or effectiveness.



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