

**OPA134  
OPA2134  
OPA4134**

## *SoundPLUS*™ High Performance AUDIO OPERATIONAL AMPLIFIERS

### FEATURES

- SUPERIOR SOUND QUALITY
- ULTRA LOW DISTORTION: 0.00008%
- LOW NOISE:  $8\text{nV}/\sqrt{\text{Hz}}$
- TRUE FET-INPUT:  $I_B = 5\text{pA}$
- HIGH SPEED:
  - SLEW RATE:  $20\text{V}/\mu\text{s}$
  - BANDWIDTH: 8MHz
- HIGH OPEN-LOOP GAIN: 120dB (600Ω)
- WIDE SUPPLY RANGE:  $\pm 2.5\text{V}$  to  $\pm 18\text{V}$
- SINGLE, DUAL, AND QUAD VERSIONS

### APPLICATIONS

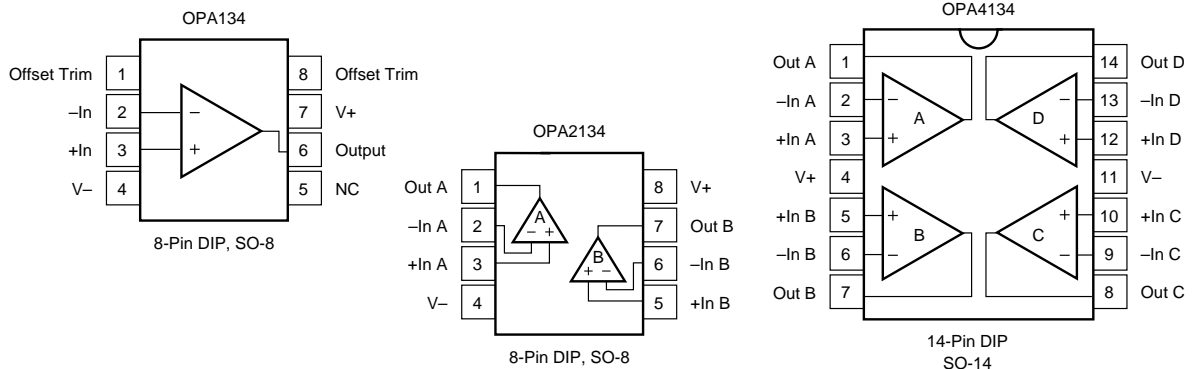
- PROFESSIONAL AUDIO AND MUSIC
- LINE DRIVERS
- LINE RECEIVERS
- MULTIMEDIA AUDIO
- ACTIVE FILTERS
- PREAMPLIFIERS
- INTEGRATORS
- CROSSOVER NETWORKS

### DESCRIPTION

The OPA134 series are ultra-low distortion, low noise operational amplifiers fully specified for audio applications. A true FET input stage was incorporated to provide superior sound quality and speed for exceptional audio performance. This in combination with high output drive capability and excellent dc performance allows use in a wide variety of demanding applications. In addition, the OPA134's wide output swing, to within 1V of the rails, allows increased headroom making it ideal for use in any audio circuit.

OPA134 op amps are easy to use and free from phase inversion and overload problems often found in common FET-input op amps. They can be operated from  $\pm 2.5\text{V}$  to  $\pm 18\text{V}$  power supplies. Input cascode circuitry provides excellent common-mode rejection and maintains low input bias current over its wide input voltage range, minimizing distortion. OPA134 series op amps are unity-gain stable and provide excellent dynamic behavior over a wide range of load conditions, including high load capacitance. The dual and quad versions feature completely independent circuitry for lowest crosstalk and freedom from interaction, even when overdriven or overloaded.

Single and dual versions are available in 8-pin DIP and SO-8 surface-mount packages in standard configurations. The quad is available in 14-pin DIP and SO-14 surface mount packages. All are specified for  $-40^\circ\text{C}$  to  $+85^\circ\text{C}$  operation. A SPICE macromodel is available for design analysis.



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# SPECIFICATIONS

At  $T_A = +25^\circ\text{C}$ ,  $V_S = \pm 15\text{V}$ , unless otherwise noted.

PARAMETER	CONDITION	OPA134PA, UA OPA2134PA, UA OPA4134PA, UA			UNITS
		MIN	TYP	MAX	
<b>AUDIO PERFORMANCE</b>					
Total Harmonic Distortion + Noise	$G = 1, f = 1\text{kHz}, V_O = 3\text{Vrms}$ $R_L = 2\text{k}\Omega$ $R_L = 600\Omega$		0.00008 0.00015		% %
Intermodulation Distortion Headroom <sup>(1)</sup>	$G = 1, f = 1\text{kHz}, V_O = 1\text{Vp-p}$ $\text{THD} < 0.01\%, R_L = 2\text{k}\Omega, V_S = \pm 18\text{V}$		-98 23.6		dB dBu
<b>FREQUENCY RESPONSE</b>					
Gain-Bandwidth Product		$\pm 15$	8		MHz
Slew Rate <sup>(2)</sup>			$\pm 20$		V/ $\mu\text{s}$
Full Power Bandwidth			1.3		MHz
Settling Time 0.1%	$G = 1, 10\text{V Step}, C_L = 100\text{pF}$		0.7		$\mu\text{s}$
0.01%	$G = 1, 10\text{V Step}, C_L = 100\text{pF}$		1		$\mu\text{s}$
Overload Recovery Time	$(V_{IN}) \cdot (\text{Gain}) = V_S$		0.5		$\mu\text{s}$
<b>NOISE</b>					
Input Voltage Noise					
Noise Voltage, $f = 20\text{Hz to } 20\text{kHz}$			1.2		$\mu\text{Vrms}$
Noise Density, $f = 1\text{kHz}$			8		nV/ $\sqrt{\text{Hz}}$
Current Noise Density, $f = 1\text{kHz}$			3		fA/ $\sqrt{\text{Hz}}$
<b>OFFSET VOLTAGE</b>					
Input Offset Voltage			$\pm 0.5$	$\pm 2$	mV
vs Temperature	$T_A = -40^\circ\text{C to } +85^\circ\text{C}$		$\pm 1$	$\pm 3^{(3)}$	mV
vs Power Supply (PSRR)	$T_A = -40^\circ\text{C to } +85^\circ\text{C}$		$\pm 2$		$\mu\text{V}/^\circ\text{C}$
Channel Separation (Dual, Quad)	$V_S = \pm 2.5\text{V to } \pm 18\text{V}$ dc, $R_L = 2\text{k}\Omega$ $f = 20\text{kHz}, R_L = 2\text{k}\Omega$	90	106 135 130		dB dB dB
<b>INPUT BIAS CURRENT</b>					
Input Bias Current <sup>(4)</sup>	$V_{CM} = 0\text{V}$		+5	$\pm 100$	pA
vs Temperature <sup>(3)</sup>			See Typical Curve	$\pm 5$	nA
Input Offset Current <sup>(4)</sup>	$V_{CM} = 0\text{V}$		$\pm 2$	$\pm 50$	pA
<b>INPUT VOLTAGE RANGE</b>					
Common-Mode Voltage Range	$V_{CM} = -12.5\text{V to } +12.5\text{V}$	(V-)+2.5	$\pm 13$	(V+)-2.5	V
Common-Mode Rejection	$T_A = -40^\circ\text{C to } +85^\circ\text{C}$	86	100 90		dB dB
<b>INPUT IMPEDANCE</b>					
Differential			$10^{13} \parallel 2$		$\Omega \parallel \text{pF}$
Common-Mode	$V_{CM} = -12.5\text{V to } +12.5\text{V}$		$10^{13} \parallel 5$		$\Omega \parallel \text{pF}$
<b>OPEN-LOOP GAIN</b>					
Open-Loop Voltage Gain	$R_L = 10\text{k}\Omega, V_O = -14.5\text{V to } +13.8\text{V}$ $R_L = 2\text{k}\Omega, V_O = -13.8\text{V to } +13.5\text{V}$ $R_L = 600\Omega, V_O = -12.8\text{V to } +12.5\text{V}$	104 104 104	120 120 120		dB dB dB
<b>OUTPUT</b>					
Voltage Output	$R_L = 10\text{k}\Omega$ $R_L = 2\text{k}\Omega$ $R_L = 600\Omega$	(V-)+0.5 (V-)+1.2 (V-)+2.2		(V+)-1.2 (V+)-1.5 (V+)-2.5	V V V
Output Current			$\pm 35$		mA
Output Impedance, Closed-Loop <sup>(5)</sup>	$f = 10\text{kHz}$		0.01		$\Omega$
Open-Loop	$f = 10\text{kHz}$		10		$\Omega$
Short-Circuit Current			$\pm 40$		mA
Capacitive Load Drive (Stable Operation)			See Typical Curve		
<b>POWER SUPPLY</b>					
Specified Operating Voltage			$\pm 15$		V
Operating Voltage Range		$\pm 2.5$		$\pm 18$	V
Quiescent Current (per amplifier)	$I_O = 0$		4	5	mA
<b>TEMPERATURE RANGE</b>					
Specified Range		-40		+85	$^\circ\text{C}$
Operating Range		-55		+125	$^\circ\text{C}$
Storage		-55		+125	$^\circ\text{C}$
Thermal Resistance, $\theta_{JA}$					
8-Pin DIP			100		$^\circ\text{C}/\text{W}$
SO-8 Surface-Mount			150		$^\circ\text{C}/\text{W}$
14-Pin DIP			80		$^\circ\text{C}/\text{W}$
SO-14 Surface-Mount			110		$^\circ\text{C}/\text{W}$

NOTES: (1)  $\text{dBu} = 20 \cdot \log(\text{Vrms}/0.7746)$  where  $\text{Vrms}$  is the maximum output voltage for which  $\text{THD} + \text{Noise}$  is less than 0.01%. See  $\text{THD} + \text{Noise}$  text. (2) Guaranteed by design. (3) Guaranteed by wafer-level test to 95% confidence level. (4) High-speed test at  $T_J = 25^\circ\text{C}$ . (5) See "Closed-Loop Output Impedance vs Frequency" typical curve.



### ABSOLUTE MAXIMUM RATINGS<sup>(1)</sup>

Supply Voltage, V+ to V- .....	36V
Input Voltage .....	(V-) -0.7V to (V+) +0.7V
Output Short-Circuit <sup>(2)</sup> .....	Continuous
Operating Temperature .....	-40°C to +125°C
Storage Temperature .....	-55°C to +125°C
Junction Temperature .....	150°C
Lead Temperature (soldering, 10s) .....	300°C

NOTES: (1) Stresses above these ratings may cause permanent damage.  
 (2) Short-circuit to ground, one amplifier per package.

### PACKAGE/ORDERING INFORMATION

PRODUCT	PACKAGE	PACKAGE DRAWING NUMBER <sup>(1)</sup>	TEMPERATURE RANGE
<b>Single</b>			
OPA134PA	8-Pin Plastic DIP	006	-40°C to +85°C
OPA134UA	SO-8 Surface-Mount	182	-40°C to +85°C
<b>Dual</b>			
OPA2134PA	8-Pin Plastic DIP	006	-40°C to +85°C
OPA2134UA	SO-8 Surface-Mount	182	-40°C to +85°C
<b>Quad</b>			
OPA4134PA	14-Pin Plastic DIP	010	-40°C to +85°C
OPA4134UA	SO-14 Surface-Mount	235	-40°C to +85°C

NOTE: (1) For detailed drawing and dimension table, please see end of data sheet, or Appendix C of Burr-Brown IC Data Book.



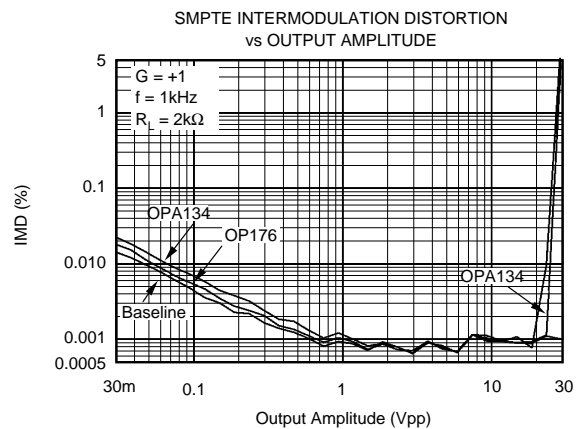
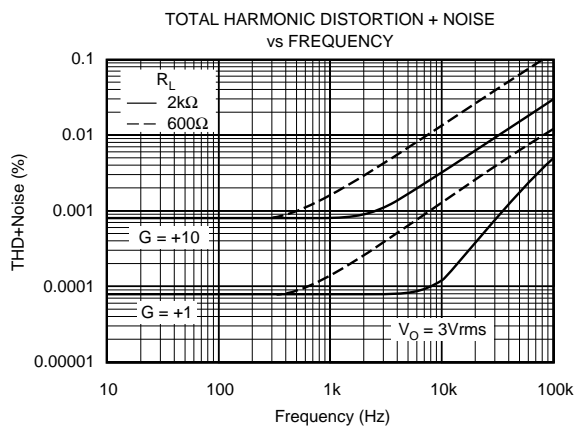
### ELECTROSTATIC DISCHARGE SENSITIVITY

This integrated circuit can be damaged by ESD. Burr-Brown recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

### TYPICAL PERFORMANCE CURVES

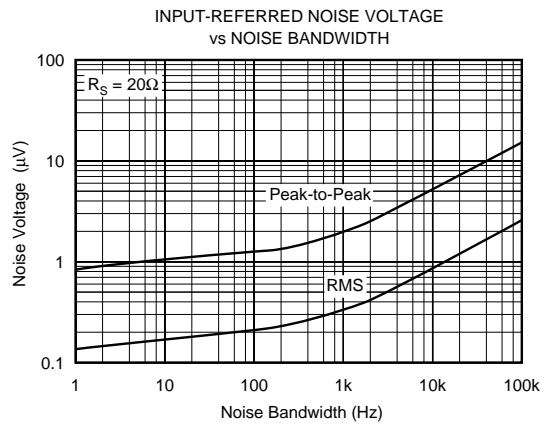
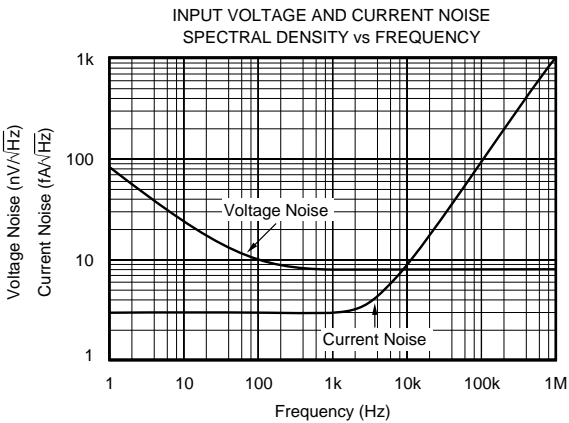
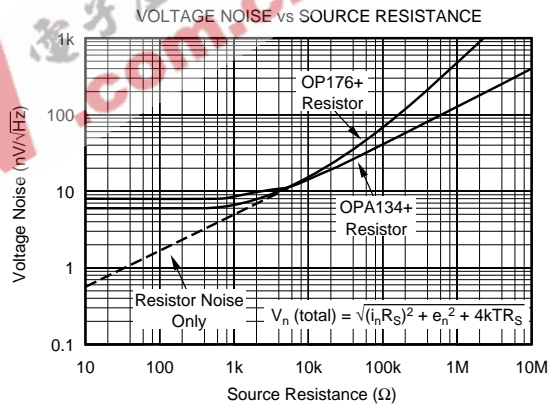
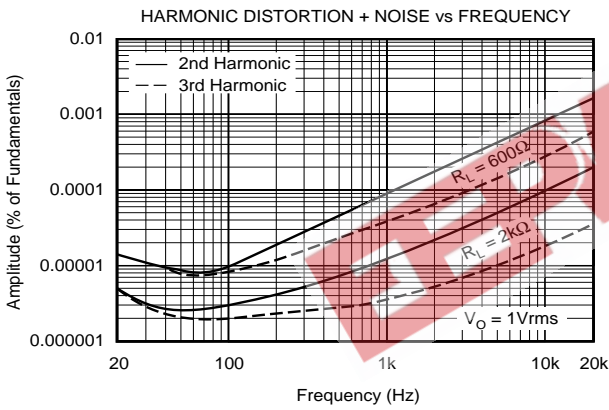
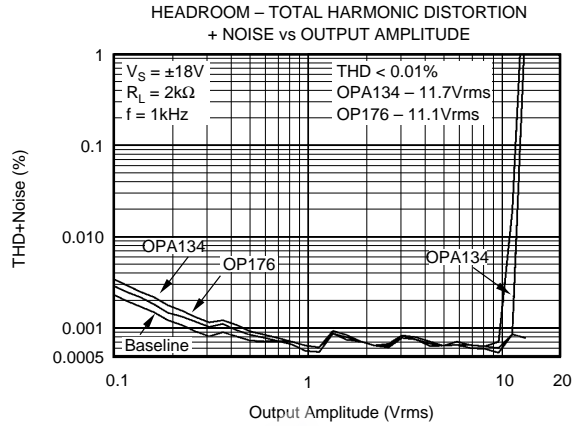
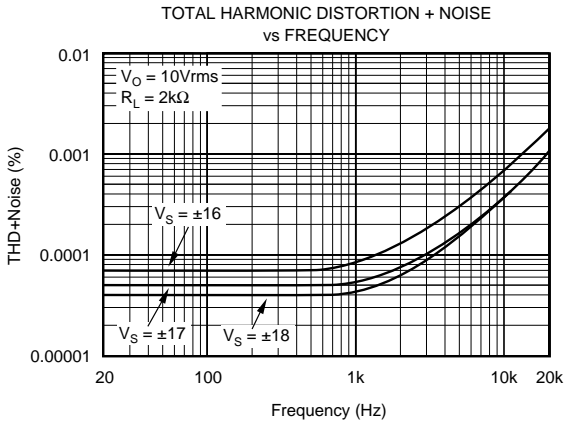
At  $T_A = +25^\circ\text{C}$ ,  $V_S = \pm 15\text{V}$ ,  $R_L = 2\text{k}\Omega$ , unless otherwise noted.



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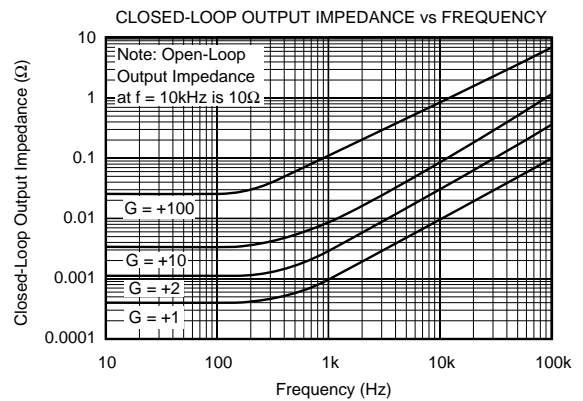
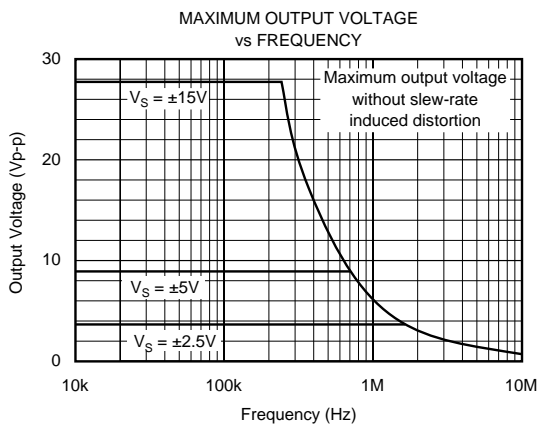
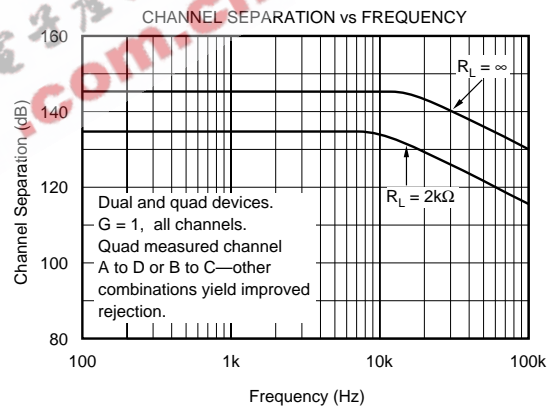
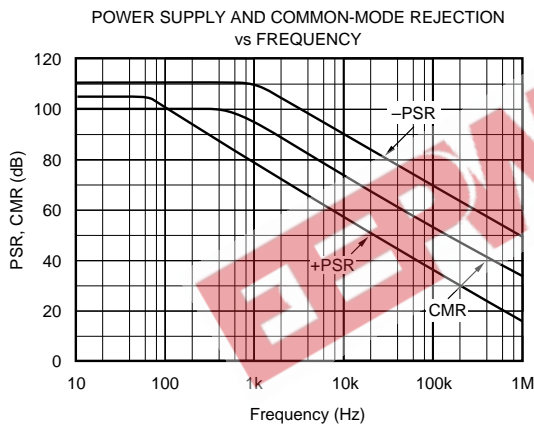
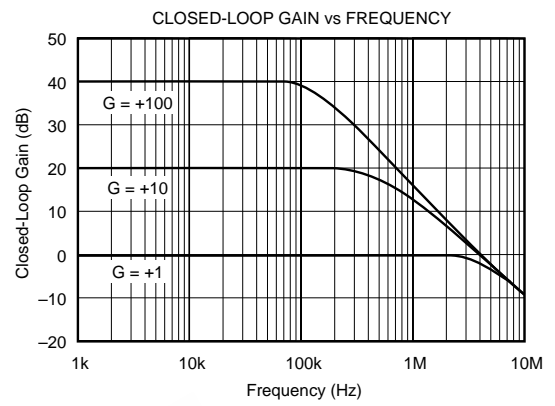
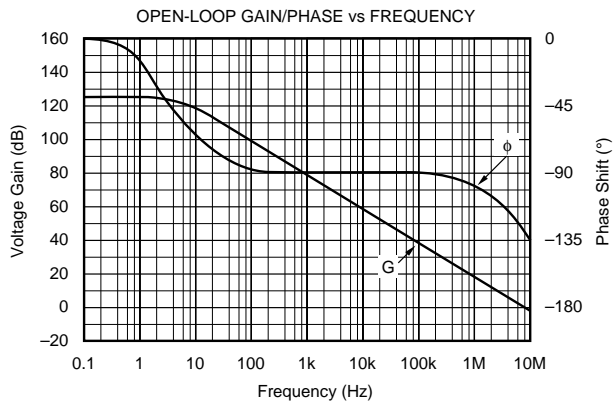
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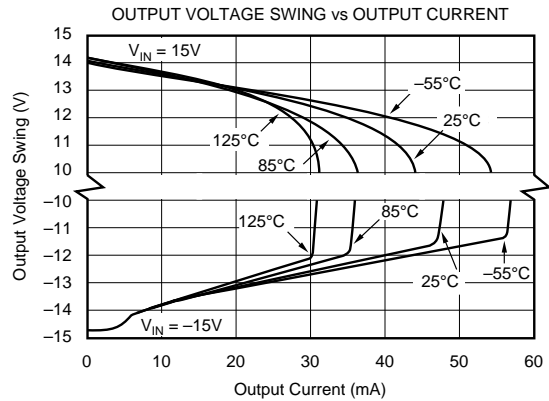
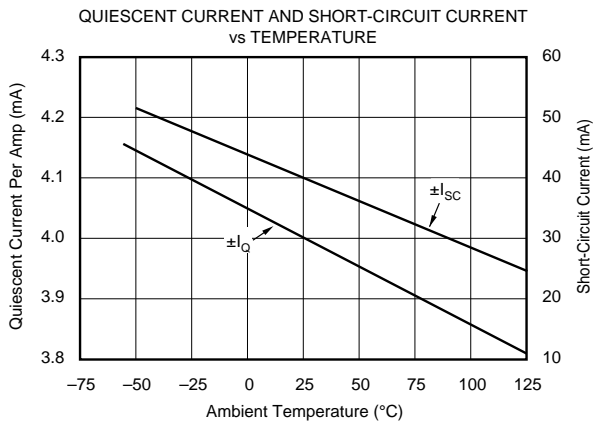
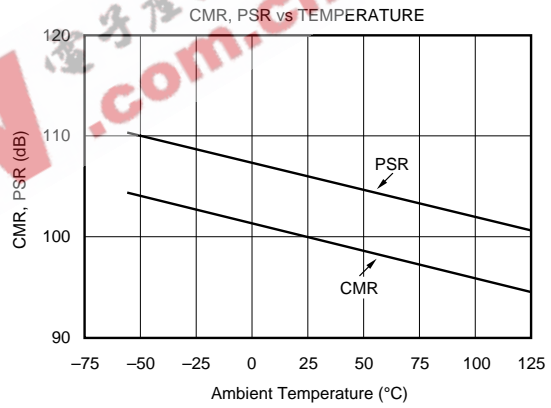
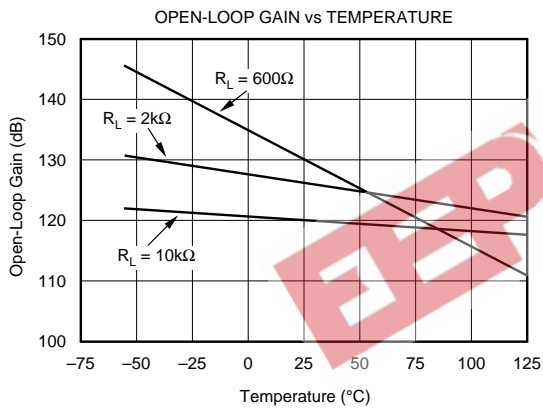
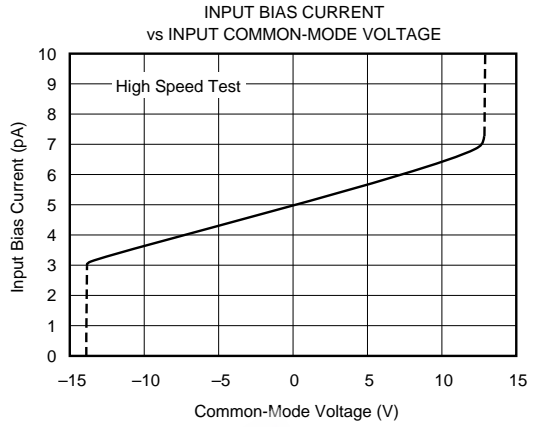
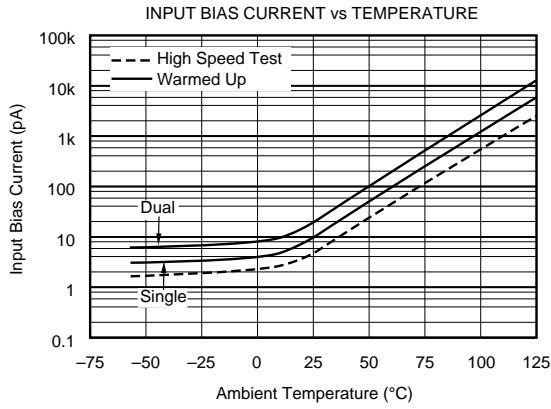
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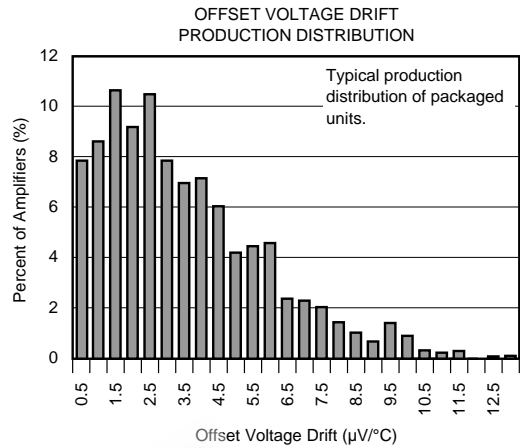
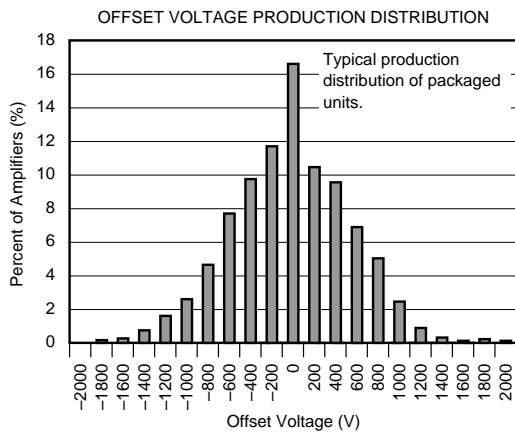
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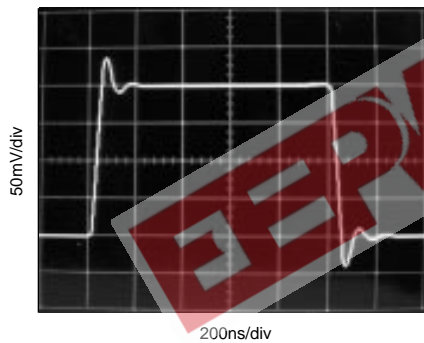


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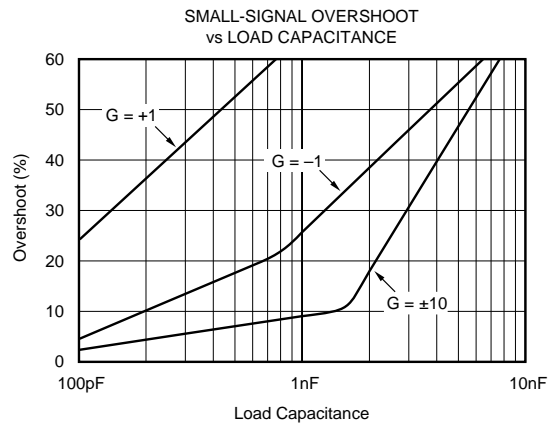
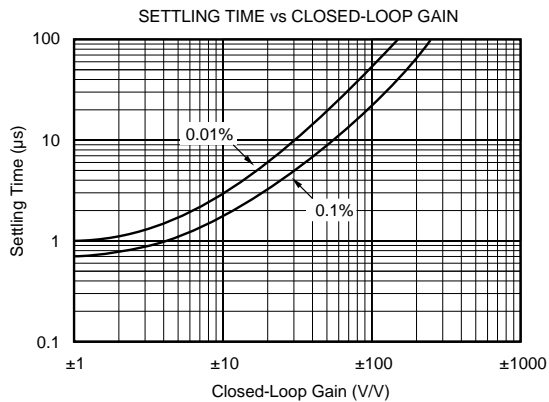
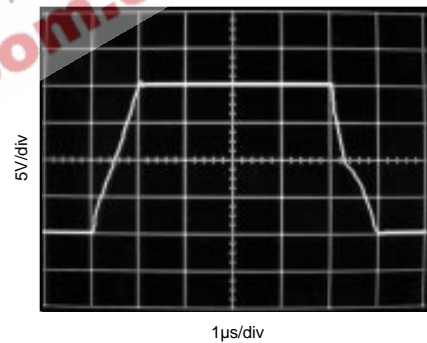
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SMALL-SIGNAL STEP RESPONSE  
 $G = 1$ ,  $C_L = 100\text{pF}$



LARGE-SIGNAL STEP RESPONSE  
 $G = 1$ ,  $C_L = 100\text{pF}$



## APPLICATIONS INFORMATION

OPA134 series op amps are unity-gain stable and suitable for a wide range of audio and general-purpose applications. All circuitry is completely independent in the dual version, assuring normal behavior when one amplifier in a package is overdriven or short-circuited. Power supply pins should be bypassed with 10nF ceramic capacitors or larger to minimize power supply noise.

### OPERATING VOLTAGE

OPA134 series op amps operate with power supplies from  $\pm 2.5V$  to  $\pm 18V$  with excellent performance. Although specifications are production tested with  $\pm 15V$  supplies, most behavior remains unchanged throughout the full operating voltage range. Parameters which vary significantly with operating voltage are shown in the typical performance curves.

### OFFSET VOLTAGE TRIM

Offset voltage of OPA134 series amplifiers is laser trimmed and usually requires no user adjustment. The OPA134 (single op amp version) provides offset trim connections on pins 1 and 8, identical to 5534 amplifiers. Offset voltage can be adjusted by connecting a potentiometer as shown in Figure 1. This adjustment should be used only to null the offset of the op amp, not to adjust system offset or offset produced by the signal source. Nulling offset could change the offset voltage drift behavior of the op amp. While it is not possible to predict the exact change in drift, the effect is usually small.

### TOTAL HARMONIC DISTORTION

OPA134 series op amps have excellent distortion characteristics. THD+Noise is below 0.0004% throughout the audio frequency range, 20Hz to 20kHz, with a 2k $\Omega$  load. In addition, distortion remains relatively flat through its wide output voltage swing range, providing increased headroom compared to other audio amplifiers, including the OP176/275.

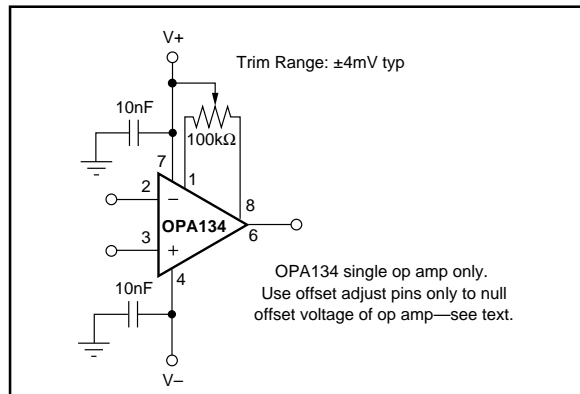


FIGURE 1. OPA134 Offset Voltage Trim Circuit.

In many ways headroom is a subjective measurement. It can be thought of as the maximum output amplitude allowed while still maintaining a very low level of distortion. In an attempt to quantify headroom, we have defined “very low distortion” as 0.01%. Headroom is expressed as a ratio which compares the maximum allowable output voltage level to a standard output level (1mW into 600 $\Omega$ , or 0.7746Vrms). Therefore, OPA134 series op amps, which have a maximum allowable output voltage level of 11.7Vrms (THD+Noise < 0.01%), have a headroom specification of 23.6dBu. See the typical curve “Headroom - Total Harmonic Distortion + Noise vs Output Amplitude.”

### DISTORTION MEASUREMENTS

The distortion produced by OPA134 series op amps is below the measurement limit of all known commercially available equipment. However, a special test circuit can be used to extend the measurement capabilities.

Op amp distortion can be considered an internal error source which can be referred to the input. Figure 2 shows a circuit which causes the op amp distortion to be 101 times greater than normally produced by the op amp. The addition of  $R_3$  to the otherwise standard non-inverting amplifier

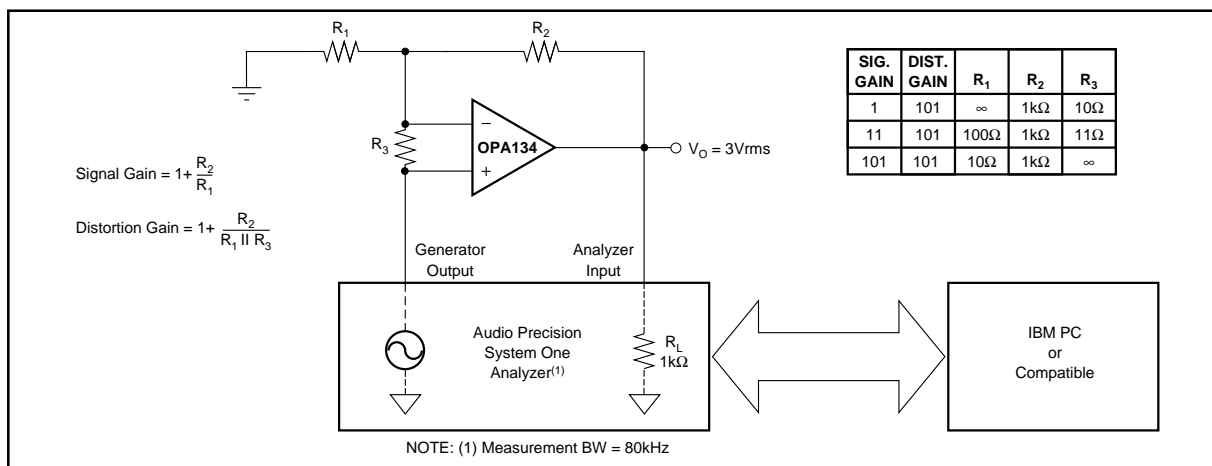


FIGURE 2. Distortion Test Circuit.



configuration alters the feedback factor or noise gain of the circuit. The closed-loop gain is unchanged, but the feedback available for error correction is reduced by a factor of 101, thus extending the resolution by 101. Note that the input signal and load applied to the op amp are the same as with conventional feedback without  $R_3$ . The value of  $R_3$  should be kept small to minimize its effect on the distortion measurements.

Validity of this technique can be verified by duplicating measurements at high gain and/or high frequency where the distortion is within the measurement capability of the test equipment. Measurements for this data sheet were made with an Audio Precision distortion/noise analyzer which greatly simplifies such repetitive measurements. The measurement technique can, however, be performed with manual distortion measurement instruments.

### SOURCE IMPEDANCE AND DISTORTION

For lowest distortion with a source or feedback network which has an impedance greater than  $2k\Omega$ , the impedance seen by the positive and negative inputs in noninverting applications should be matched. The p-channel JFETs in the FET input stage exhibit a varying input capacitance with applied common-mode input voltage. In inverting configurations the input does not vary with input voltage since the inverting input is held at virtual ground. However, in noninverting applications the inputs do vary, and the gate-to-source voltage is not constant. The effect is increased distortion due to the varying capacitance for unmatched source impedances greater than  $2k\Omega$ .

To maintain low distortion, match unbalanced source impedance with appropriate values in the feedback network as shown in Figure 3. Of course, the unbalanced impedance may be from gain-setting resistors in the feedback path. If the parallel combination of  $R_1$  and  $R_2$  is greater than  $2k\Omega$ , a matching impedance on the noninverting input should be used. As always, resistor values should be minimized to reduce the effects of thermal noise.

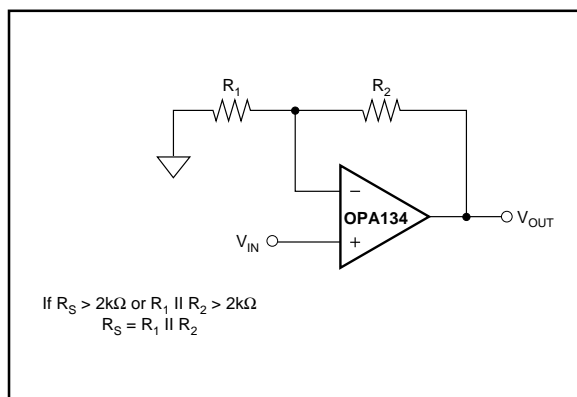


FIGURE 3. Impedance Matching for Maintaining Low Distortion in Non-Inverting Circuits.

### NOISE PERFORMANCE

Circuit noise is determined by the thermal noise of external resistors and op amp noise. Op amp noise is described by two parameters—noise voltage and noise current. The total noise is quantified by the equation:

$$V_n(\text{total}) = \sqrt{(i_n R_S)^2 + e_n^2 + 4kTR_s}$$

With low source impedance, the current noise term is insignificant and voltage noise dominates the noise performance. At high source impedance, the current noise term becomes the dominant contributor.

Low noise bipolar op amps such as the OPA27 and OPA37 provide very low voltage noise at the expense of a higher current noise. However, OPA134 series op amps are unique in providing very low voltage noise and very low current noise. This provides optimum noise performance over a wide range of sources, including reactive source impedances, refer to the typical curve, “Voltage Noise vs Source Resistance.” Above  $2k\Omega$  source resistance, the op amp contributes little additional noise—the voltage and current terms in the total noise equation become insignificant and the source resistance term dominates. Below  $2k\Omega$ , op amp voltage noise dominates over the resistor noise, but compares favorably with other audio op amps such as OP176.

### PHASE REVERSAL PROTECTION

OPA134 series op amps are free from output phase-reversal problems. Many audio op amps, such as OP176, exhibit phase-reversal of the output when the input common-mode voltage range is exceeded. This can occur in voltage-follower circuits, causing serious problems in control loop applications. OPA134 series op amps are free from this undesirable behavior even with inputs of 10V beyond the input common-mode range.

### POWER DISSIPATION

OPA134 series op amps are capable of driving  $600\Omega$  loads with power supply voltage up to  $\pm 18V$ . Internal power dissipation is increased when operating at high supply voltages. Copper leadframe construction used in OPA134 series op amps improves heat dissipation compared to conventional materials. Circuit board layout can also help minimize junction temperature rise. Wide copper traces help dissipate the heat by acting as an additional heat sink. Temperature rise can be further minimized by soldering the devices to the circuit board rather than using a socket.

### OUTPUT CURRENT LIMIT

Output current is limited by internal circuitry to approximately  $\pm 40mA$  at  $25^\circ C$ . The limit current decreases with increasing temperature as shown in the typical performance curve “Short-Circuit Current vs Temperature.”