INTEGRATED CIRCUITS



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OQ2538HP; OQ2538U

FEATURES

- Differential 100 Ω outputs for direct connection to Current-Mode Logic (CML) inputs
- Wide bandwidth (3 GHz)
- 48.5 dB limiting gain
- Noise figure typically 11 dB
- Automatic offset compensation
- Input level-detection circuits for Automatic Gain Control (AGC) and Loss Of Signal (LOS) detection
- Low power dissipation (typically 270 mW)
- Single -4.5 V supply voltage
- Low cost LQFP48 plastic package.

APPLICATIONS

- Main amplifier in Synchronous Digital Hierarchy (SDH) and Synchronous Optical Network (SONET) systems for short, medium and long haul optical transmission
- Level detector for laser diode control loops
- Wideband RF gain block with internal level detectors.

ORDERING INFORMATION

GENERAL DESCRIPTION

The OQ2538HP is a limiting amplifier IC intended for use as the main amplifier in 2.5 Gbits/s Non-Return to Zero (NRZ) transmission systems (SDH/SONET).

Comprised of four amplifier stages with a total gain of 48.5 dB, it provides for a wide input signal dynamic range at a constant CML-compatible output level.

Two level-detection circuits are provided for monitoring AGC and LOS input signal levels. An internal automatic offset compensation circuit eliminates offset in the amplifier chain.



TYPE	PACKAGE				
NUMBER	NAME	DESCRIPTION	VERSION		
OQ2538HP	LQFP48	plastic low profile quad flat package; 48 leads; body $7 \times 7 \times 1.4$ mm	SOT313-2		
OQ2538U	_	are die; dimensions 2070 × 2070 × 380 μm			

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BLOCK DIAGRAM



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PINNING

SYMBOL	PIN (OQ2538HP)	PAD (OQ2538U)	TYPE ⁽¹⁾	DESCRIPTION
V _{EE}	1, 12, 13, 24, 25, 36, 37, 48	2, 3, 11, 12, 28, 29 ⁽²⁾	S	negative power supply
n.c.	2, 11, 14, 15, 23, 26, 27, 35, 38, 40, 46, 47	20, 22 ⁽³⁾	_	not connected
AGC	3	30	0	rectifier A output
GND	4, 5, 7, 9, 10, 16, 17, 20, 28, 29, 31, 33, 34, 39, 41, 42	$1, 4, 5, 8, 13, 14, \\16, 18, 19, 21, \\23, 24, 31, 32, \\34, 36^{(2)}$	S	ground
INQ	6	33	I	main amplifier inverting input
IN	8	35	I	main amplifier input
LOSDC	18	6	0	rectifier B reference output
LOS	19	7	0	rectifier B output
REF	21	9	0	band gap reference
CAPA	22	10	А	pin for connecting band gap reference decoupling capacitor
OUTQ	30	15	0	main amplifier inverted output
OUT	32	17	0	main amplifier output
AGCDC	43	25	0	rectifier A reference output
COFFQ	44	26	A	pin for connecting automatic offset control capacitor (return)
COFF	45	27	A	pin for connecting automatic offset control capacitor
N				

Notes

1. Pin type abbreviations: O = Output, I = Input, S = power Supply and A = Analog function.

2. All GND and V_{EE} pads must be bonded; do not leave one single GND or V_{EE} pad unconnected!

3. Pads denoted 'n.c.' should not be connected. Connections to these pads degrade device performance.

SDH/SONET STM16/OC48 main amplifiers OQ2538HP; OQ2538U



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FUNCTIONAL DESCRIPTION

The OQ2538HP is comprised of four DC-coupled amplifier stages along with additional circuitry for offset compensation and level detection.

The first amplifier stage contains a modified Cherry/Hooper amplifying cell with high gain (approximately 20 dB) and a wide bandwidth. Special attention is paid to minimizing the equivalent input noise at this stage, thus reducing the overall noise level. Additional feedback is applied at the second and third stages, improving isolation and reducing the gain to 14 dB per stage. The last stage is an output buffer, a unity gain amplifier, with an output impedance of 100 Ω .

The total gain of the OQ2538HP amounts to 48.5 dB, thus providing a constant CML-compatible output signal over a wide input signal range.

Two rectifier circuits are used to measure the input signal level. Two separate RF preamplifiers are used to generate the voltage gain needed to obtain a suitable rectifier output voltage. For rectifier A the gain is approximately 18 dB, for rectifier B it is about 14 dB. The output of rectifier A can be used for AGC at the preamplifier stage in front of the OQ2538HP. The output of rectifier B can be used for LOS detection. There is a linear relationship between the rectifier output voltage and the input signal level provided the amplifiers are not saturated.

Because the four gain stages are DC-coupled and provide a high overall gain, the effect of the input offset can be considerable. The OQ2538HP features an internal offset compensation circuit for eliminating the input offset. The bandwidth of the offset control loop is determined by an external capacitor.

COFF and COFFQ offset compensation

Automatic offset compensation eliminates the input offset of the OQ2538HP. This offset cancellation influences the low frequency gain of the amplifier stages. With a capacitance of 100 nF between COFF and COFFQ the loop bandwidth will be less than 1.5 kHz, small enough to have no influence on amplifier gain over the frequencies of interest. If the capacitor was omitted, the loop bandwidth would be greater than 30 MHz, which would influence the input signal gain. The loop bandwidth can be calculated from the following formula:

$$f_{loop} = \frac{1}{2\pi \times 1250 \,\Omega \times C_{ext}}$$
(1)

where C_{ext} is the capacitance connected between COFF and COFFQ.

REF and CAPA band gap output and decoupling capacitance

To reduce band gap noise levels, a 1 nF decoupling capacitor on CAPA is recommended. Since the band gap is referenced to the negative power supply, the decoupling capacitor should be connected between CAPA and V_{EE} .

The band gap voltage is present on pin REF for test purposes only. It is not intended to serve as an external reference.

RF input and output connections

Striplines, or microstrips, with an odd mode characteristic impedance of $Z_{o(odd)} = 50 \ \Omega$ must be used for the differential RF connections on the PCB. This applies to both the input signal pair IN and INQ and to the output signal pair OUT and OUTQ. The two lines in each pair should have the same length.

RF input matching circuit

The input circuit for pins IN and INQ contains internal 100 Ω resistors decoupled to ground via an internal common mode 6 pF capacitor. The topology is depicted in Fig.3.



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An external 200 Ω resistor between IN and INQ is recommended in order to match the inputs to a differential transmission line, coupled microstrip or stripline with an odd mode impedance $Z_{o(odd)} = 50 \Omega$, as shown in Fig.4.



For single-ended excitation, separate matching networks on IN and INQ, as depicted in Fig.5, achieve optimum matching. Care should be taken to avoid DC loading, since the OQ2538HP controls its own DC input voltage. The resistors on the unused input INQ may be combined for convenience.



In both cases, the essence of good matching is the equity of the circuitry on both input pins. The impedance seen on pins IN and INQ should be as equal as possible. For more information see *"Application Note AN96051"* describing the OM5801 STM16 demo board.

RF output matching circuit

Matching of the main amplifier outputs, OUT and OUTQ, is not mandatory. In most applications, the receiving end of the transmission line will be properly matched, so very little reflection will occur. Matching the transmitting end to absorb these reflections is only recommended for very sensitive applications. In such cases, 100Ω pull-up resistors should be connected from OUT and OUTQ to ground, as close as possible to the IC pins. These matching resistors will not be needed in most applications, however. The output circuit of the OQ2538HP is depicted in Fig.6. For more information see *"Application Note AN96051"* describing the OM5801 STM16 demo board.



Product specification

SDH/SONET STM16/OC48 main amplifiers

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RF gain and group delay measurements

The measurement set-up shown in Fig.7 was used to measure the single-ended small signal gain as specified in Chapter "Characteristics". Since the network analyzer can only perform single-ended measurements, the single-ended matching scheme described above is used to match the inputs of the OQ2538HP to 50 Ω . For greater accuracy, the outputs are also matched. The gain measured with this set-up is denoted by S21. Graphs of typical S₂₁ and group delay characteristics are shown in Figs 8 and 9. The OQ2538HP test PCB used for these measurements can be supplied on request.

Although the differential voltage gain of the OQ2538HP cannot be measured directly, it can be calculated from S₂₁. The differential voltage gain is 6 dB greater than the measured S_{21} value, typically 46 dB (40 + 6 dB). If the 100 Ω matching resistors on the output are omitted, the differential voltage gain is increased by a further 2.4 dB, typically to 48.4 dB. This is due to the fact that the output load is increased from 25 to 33 Ω , so the output voltage is increased by a factor of 1.32 (2.4 dB).

When performing S₂₁ measurements make sure the input power level is around -50 dBm, as indicated in Fig.7 (port 1 of the network analyzer). For correct measurement results the OQ2538 should not be limiting the input signal, but operate in its linear region. This can be achieved by using a very small input signal level of -50 dBm.

6 GHz NETWORK ANALYZER S-PARAMETER TEST SET P = 50 dBmPORT 1 PORT 2 $Z_0 = 50 \ \Omega$ $Z_0 = 50 \Omega$ OQ2538HP test PCB 100 pF 50 Ω semi rigid 50 Ω semi rigid -11 IN 100 pF 50 Ω semi rigid 50 Ω semi rigid INQ OUTQ -11 6 50 Ω SMA $50 \Omega SMA$ 100 Ω 100 Ω 100 Ω 100 Ω termination termination -4.5 V VEE MGM111

Fig.7 S₂₁ and group delay measurement set-up.

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Noise figure measurements

The noise figure is the ratio of signal-to-noise ratio at the input (S_i/N_i) to signal-to-noise ratio at the output (S_o/N_o) of the amplifier. This definition is true for both single-ended and differential amplifiers, provided the correct values for S_i/N_i and S_o/N_o are substituted in the formula. The noise figure is measured using the differential set-up shown in Fig.10. The total noise on the output (No in dBm) is measured using the spectrum analyzer at the frequency of interest. From this value, the actual (differential) noise figure for that frequency (spot noise figure) can be calculated using the following formula:

$$\mathsf{F} = \frac{\mathsf{S}_i / \mathsf{N}_i}{\mathsf{S}_o / \mathsf{N}_o} = \frac{\mathsf{N}_o}{2 \cdot \mathsf{S}_{21} \cdot \mathsf{N}_i} = \frac{\mathsf{N}_o}{2 \cdot \mathsf{S}_{21} \cdot \mathsf{kT}}$$

The factor 2 in the denominator is present to compensate for the fact that S₂₁ is the single-ended power gain,

whereas the differential power gain is applicable in this situation. Ni can be replaced with the available noise power at the input, which is kT under matched conditions (k is Boltzmann's constant). The formula expressed in dBm makes calculation easier:

 $F = N_0 - (S_{21} + 3) + 173.8$ [dB],

assuming log(kT) is -173.8 dBm (T = 298 K) and No measured in 1 Hz bandwidth and expressed in dBm. For the OQ2538HP, in the differential configuration (including the 100 Ω matching resistors), this yields a typical noise figure of 11 dB.

While the performance of this measurement set-up cannot match that of a dedicated noise analysis system, the results are comparable for an amplifier with a noise figure of 11 dB.



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AGC and AGCDC level detection

When using rectifier A as an input signal level detector, the AGC and AGCDC pins must be decoupled to ground with 100 nF capacitors. The AGCDC output is intended as a reference voltage against which the actual AGC output voltage can be compared. This voltage difference, $V_{AGC} - V_{AGCDC}$, can be used as a control input in an AGC loop. A graph depicting output voltage difference as a function of the input signal level (typical) is shown in Fig.11. Note that an input signal with the specified peak-to-peak value is applied to both IN and INQ inputs, but with complementary phase.

LOS and LOSDC level detection

The output of rectifier B can be used for LOS detection. The LOSDC output provides a reference voltage against which the voltage at the LOS output can be compared. The voltage difference $V_{LOS} - V_{LOSDC}$ can be used as input to a LOS detection circuit. Both outputs need to be decoupled using 100 nF capacitors. A graph depicting $V_{LOS} - V_{LOSDC}$ as a function of the input signal level (typical) is shown in Fig.12. Note that an input signal with the specified peak-to-peak value is applied to both IN and INQ inputs, but with complementary phase.



Grounding and power supply decoupling

The ground connection on the PCB needs to be a large copper area fill connected to a common ground plane with as low inductance as possible, preferably positioned directly underneath the LQFP48 package. The large area fill will improve heat transfer to the PCB and thus aid IC cooling.

All V_{EE} pins (two at each corner) need to be connected to a common supply plane with as low inductance as possible. This plane should be decoupled to ground. To avoid high frequency resonance, multiple bypass capacitors should not be mounted at the same location. To minimize low frequency switching noise in the vicinity of the OQ2538HP, the power supply line should be filtered once using an LC-circuit with a low cut-off frequency (see Fig.14).

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Using alternative supply voltages

Although the OQ2538HP is intended to be used with a single -4.5 V supply voltage, a slightly modified -5 V supply can also be used. By connecting a Schottky diode between the V_{EE} power supply line and the IC, an additional 0.5 V voltage drop is obtained, bringing the supply voltage on the pins of the OQ2538HP within the specified range. A BAS85 Schottky diode is recommended. A -5 V application schematic is shown in Fig.15.

Extrapolating from this case, a +5 V application is also possible. However, care should be taken with the RF transmission lines. The on-chip signals refer to the GND pins, which become the positive supply pins in a +5 V application. The external transmission lines will most likely be referenced to system ground (V_{EE} pins). The RF signals will change from one reference plane to another at the interface to the RF input and output pins. The positive supply application is very vulnerable to interference at this point. For a successful +5 V application, special care should be taken when designing board layout to reduce the influence of interference and keep the positive supply as clean as possible.

ESD protection

Exceptions have been made to the standard ESD protection scheme in order to achieve high frequency performance. The inputs IN and INQ and the outputs OUT and OUTQ have **no protection** against ESD. All other pins have a standard ESD protection structure, capable of withstanding 2 kV Human Body Model (HBM) zappings.

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LIMITING VALUES

In accordance with the Absolute Maximum Rating System (IEC 134).

SYMBOL	PARAMETER	CONDITIONS	MIN.	MAX.	UNIT
V _{EE}	negative supply voltage		-6.0	+0.5	V
ΔV_{I}	input voltage difference	note 1	-600	+600	mV
I _{IN} , I _{INQ}	input current		-2.0	+2.0	mA
I _n	DC current				
	pins 30 and 32		-6	+10	mA
	pins 3, 18, 19 and 43		-3	+3	mA
	pin 21		-2	+2	mA
	pins 44 and 45		-1	+1	mA
	pin 22		-0.1	+0.1	mA
P _{tot}	total power dissipation		-	380	mW
Tj	junction temperature			150	°C
T _{stg}	storage temperature		-65	+150	°C

1. $\Delta V_{I} = V_{IN} - V_{INQ}$ (AC only). The DC level is internally controlled. **HANDLING** Precautions should be taken to consist. Precautions should be taken to avoid damage through electrostatic discharge. This is particularly important during assembly and handling of the bare die. Additional safety can be obtained by bonding the VEE and GND pads first, the remaining pads may then be bonded to their external connections in any order (see also Section "ESD protection").

THERMAL CHARACTERISTICS

SYMBOL	DESCRIPTION	CONDITIONS	VALUE	UNIT
R _{th(j-s)}	thermal resistance from junction to solder point		15	K/W
R _{th(j-a)}	thermal resistance from junction to ambient	note 1	65	K/W

Note

1. R_{th(i-a)} will be in the application from 15 to 65 K/W, dependent on the PCB layout.

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CHARACTERISTICS

At nominal supply voltages; T_{amb} = -40 to +85 °C; 50 Ω measuring environment.

SYMBOL	PARAMETER	CONDITIONS	MIN.	TYP.	MAX.	UNIT
V _{EE}	negative supply voltage		-4.725	-4.5	-4.275	V
I _{EE}	negative supply current		-	60	80	mA
P _{tot}	total power dissipation	note 1	-	270	380	mW
T _{amb}	operating ambient temperature	note 2	-40	_	+85	°C
Tj	operating junction temperature		-40	_	+120	°C
Main amp	ifier inputs: IN and INQ; note 3			•	·	•
V _{i(sens)}	input sensitivity	note 4	-	0.5	2.5	mV
V _{i(p-p)}	signal voltage swing (peak-to-peak value)	note 4	2.5	-	600	mV
VI	DC input voltage	note 5	-2.4	-2.1	-1.7	V
V _{IO}	input offset voltage	note 6	a	0.2	-	mV
Zi	single-ended input impedance	note 7	3 Th	100	_	Ω
S ₂₁	single-ended small signal gain	note 8 🛛 🐁 😵	34	40	-	dB
G _{v(dif)}	differential voltage gain	note 9	-0-	48.5	-	dB
No	output noise power	note 10	_	-120	-	dBm
F	noise figure	note 10	-	11	-	dB
B _{-3dB}	3 dB bandwidth		2.4	3.0	-	GHz
Rectifier o	utputs: AGC and AGCDC; note 11					
V _{O(ref)}	DC reference voltage	open output	-3.3	-3.0	-2.5	V
V _{i(p-p)}	input voltages on pins IN and INQ for linear rectifier output (peak-to-peak value)		12.5	-	60	mV
ΔV	maximum input signal level related voltage difference	note 12	-	400	_	mV
V _{OO}	output offset voltage	note 13	-5	_	+5	mV
Rectifier o	utputs: LOS and LOSDC; note 11					
V _{O(ref)}	DC reference voltage	open output	-3.4	-3.1	-2.6	V
V _{i(p-p)}	input voltages on pins IN and INQ for linear recitifier output (peak-to-peak value)		2.5	-	9	mV
ΔV	maximum input signal level related voltage difference	note 12	-	450	-	mV
V _{OO}	output offset voltage	note 13	–15	-	+15	mV
Automatic offset compensation lowpass filter: COFF and COFFQ						
Vo	DC output voltage	open output	-2.4	-2.1	-1.7	V
R	offset compensation filter resistance		-	1250	_	Ω
Band gap	reference: REF					
Vo	band gap voltage	referenced to V _{EE} ; open output: note 14	1.1	1.3	1.5	V

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SYMBOL	PARAMETER	CONDITIONS	MIN.	TYP.	MAX.	UNIT
Band gap reference decoupling: CAPA						
Vo	decoupling voltage	referenced to V _{EE} ; open output	_	2.9	_	V
Main ampl	Main amplifier outputs: OUT and OUTQ; note 15					
V _{OH}	HIGH-level output voltage		-20	-5	0	mV
V _{OL}	LOW-level output voltage	note 16	-280	-200	-140	mV
t _r	differential output rise time	input signal >2.5 mV (p-p)	-	100	150	ps
t _f	differential output fall time	input signal >2.5 mV (p-p)	-	100	150	ps
Zo	single-ended output impedance	see Fig.6	83	100	117	Ω

Notes

- 1. No special cooling is required in the application if the total thermal resistance R_{th(i-a)} is less than 90 K/W.
- 2. The temperature of the PCB in the vicinity of the IC is taken to be the ambient temperature.
- 3. The input signal must be AC-coupled to the inputs through a coupling capacitance >22 nF.
- 4. V_{i(p-p)} is the input signal on IN and INQ for full output clipping. It is assumed that both inputs carry a complementary signal of the specified peak-to-peak value. The lower specified limit is usually called the input sensitivity. This value is defined as a 20% increase in rise and fall times when compared to rise and fall times with a complementary input signal of 10 mV (p-p) applied to IN and INQ.
- 5. The DC voltage is fixed internally; only AC-coupling of the input signal is allowed.
- 6. $V_{IO} = |V_{IN} V_{INQ}|$
- 7. See Section "RF input matching circuit" for detailed information.
- 8. All signal ports are AC-matched to 50 Ω and are measured at 1 GHz (see Fig.7). Flatness deviations are within ±3 dB over the entire bandwidth.
- 9. See Section "RF gain and group delay measurements".
- 10. F is the noise figure for a differential application and is measured at 1 GHz. See Section "Noise figure measurements".
- 11. An external 100 nF capacitor is connected at each output to remove any spurious high frequency signals. Any circuitry driven from these pins must have an input impedance >50 k Ω .
- 12. Voltage difference between AGC (LOS) and AGCDC (LOSDC), measured with a differential square wave input signal of 600 mV (p-p) on IN and INQ.
- 13. The offset is measured with inputs IN and INQ shorted together.
- 14. The band gap voltage may not be used as an external reference.
- 15. Both outputs are connected to ground through a 50 Ω load resistance and carry complementary signals.
- 16. The output levels are dependent on load impedance. The specified values assume an external load impedance of 50 Ω . If the external 100 Ω matching resistors are connected at pins OUT and OUTQ, the output levels will fall to 75% of the specified values (see also Section "RF gain and group delay measurements").

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APPLICATION INFORMATION



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BONDING PAD LOCATIONS



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Table 1Bonding pad locations. All x/y coordinates
represent the position of the centre of the pad
with respect to the centre of the die (see
Fig.16).

SAMBOI		COORDINATES		
STWIDUL	FAD	x	у	
GND	1	-900	-700	
V _{EE}	2	-900	-900	
V _{EE}	3	-700	-900	
GND	4	-500	-900	
GND	5	-300	-900	
LOSDC	6	-100	-900	
LOS	7	+100	-900	
GND	8	+300	-900	
REF	9	+500	-900	
CAPA	10	+700	-900	
V _{EE}	11	+900	-900	
V _{EE}	12	+900	-700	
GND	13	+900	-500	
GND	14	+900	-300	
OUTQ	15	+900	-100	
GND	16	+900	+100	
OUT	17	+900	+300	
GND	18	+900	+500	

SYMBOL	BAD	COORD	INATES	
STIVIDUL	FAD	x	У	
GND	19	+900	+700	
n.c.	20	+900	+900	
GND	21	+700	+900	
n.c.	22	+500	+900	
GND	23	+300	+900	
GND	24	+100	+900	
AGCDC	25	-100	+900	
COFFQ	26	-300	+900	
COFF	27	-500	+900	
V _{EE}	28	-700	+900	
VEE & P	29	-900	+900	
AGC	30	-900	+700	
GND	31	-900	+500	
GND	32	-900	+300	
INQ	33	-900	+100	
GND	34	-900	-100	
IN	35	-900	-300	
GND	36	-900	-500	

Table 2 Physical characteristics of bare die

PARAMETER	VALUE
Glass passivation	0.8 μ m silicon nitride on top of 0.9 μ m PSG (PhosphoSilicate Glass)
Bonding pad dimension	minimum dimension of exposed metallization is 90 \times 90 μm (pad size = 100 \times 100 μm)
Metallization	1.8 μm AlCu (1% Cu)
Thickness	380 μm nominal
Size	$2.070 \times 2.070 \text{ mm} (4.285 \text{ mm}^2)$
Backing	silicon; electrically connected to V_{EE} potential through substrate contacts
Attache temperature	<440 °C; recommended die attache is glue
Attache time	<15 s

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PACKAGE OUTLINE



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SOLDERING

Introduction

There is no soldering method that is ideal for all IC packages. Wave soldering is often preferred when through-hole and surface mounted components are mixed on one printed-circuit board. However, wave soldering is not always suitable for surface mounted ICs, or for printed-circuits with high population densities. In these situations reflow soldering is often used.

This text gives a very brief insight to a complex technology. A more in-depth account of soldering ICs can be found in our *"Data Handbook IC26; Integrated Circuit Packages"* (order code 9398 652 90011).

Reflow soldering

Reflow soldering techniques are suitable for all LQFP packages.

Reflow soldering requires solder paste (a suspension of fine solder particles, flux and binding agent) to be applied to the printed-circuit board by screen printing, stencilling or pressure-syringe dispensing before package placement.

Several methods exist for reflowing; for example, infrared/convection heating in a conveyor type oven. Throughput times (preheating, soldering and cooling) vary between 50 and 300 seconds depending on heating method. Typical reflow peak temperatures range from 215 to 250 °C.

Wave soldering

Wave soldering is **not** recommended for LQFP packages. This is because of the likelihood of solder bridging due to closely-spaced leads and the possibility of incomplete solder penetration in multi-lead devices.

CAUTION

Wave soldering is NOT applicable for all LQFP packages with a pitch (e) equal or less than 0.5 mm.

If wave soldering cannot be avoided, for LQFP packages with a pitch (e) larger than 0.5 mm, the following conditions must be observed:

- A double-wave (a turbulent wave with high upward pressure followed by a smooth laminar wave) soldering technique should be used.
- The footprint must be at an angle of 45° to the board direction and must incorporate solder thieves downstream and at the side corners.

During placement and before soldering, the package must be fixed with a droplet of adhesive. The adhesive can be applied by screen printing, pin transfer or syringe dispensing. The package can be soldered after the adhesive is cured.

Maximum permissible solder temperature is 260 °C, and maximum duration of package immersion in solder is 10 seconds, if cooled to less than 150 °C within 6 seconds. Typical dwell time is 4 seconds at 250 °C.

A mildly-activated flux will eliminate the need for removal of corrosive residues in most applications.

Repairing soldered joints

Fix the component by first soldering two diagonallyopposite end leads. Use only a low voltage soldering iron (less than 24 V) applied to the flat part of the lead. Contact time must be limited to 10 seconds at up to 300 °C. When using a dedicated tool, all other leads can be soldered in one operation within 2 to 5 seconds between 270 and 320 °C.

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DEFINITIONS

Data sheet status			
Objective specification	This data sheet contains target or goal specifications for product development.		
Preliminary specification	This data sheet contains preliminary data; supplementary data may be published later.		
Product specification	This data sheet contains final product specifications.		
Limiting values			
Limiting values given are in accordance with the Absolute Maximum Rating System (IEC 134). Stress above one or more of the limiting values may cause permanent damage to the device. These are stress ratings only and operation of the device at these or at any other conditions above those given in the Characteristics sections of the specification is not implied. Exposure to limiting values for extended periods may affect device reliability.			
Application information			

Where application information is given, it is advisory and does not form part of the specification.

LIFE SUPPORT APPLICATIONS

These products are not designed for use in life support appliances, devices, or systems where malfunction of these products can reasonably be expected to result in personal injury. Philips customers using or selling these products for use in such applications do so at their own risk and agree to fully indemnify Philips for any damages resulting from such improper use or sale.

BARE DIE DISCLAIMER

All die are tested and are guaranteed to comply with all data sheet limits up to the point of wafer sawing for a period of ninety (90) days from the date of Philips' delivery. If there are data sheet limits not guaranteed, these will be separately indicated in the data sheet. There is no post waffle pack testing performed on individual die. Although the most modern processes are utilized for wafer sawing and die pick and place into waffle pack carriers, Philips Semiconductors has no control of third party procedures in the handling, packing or assembly of the die. Accordingly, Philips Semiconductors assumes no liability for device functionality or performance of the die or systems after handling, packing or assembly of the die. It is the responsibility of the customer to test and qualify their application in which the die is used.

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